

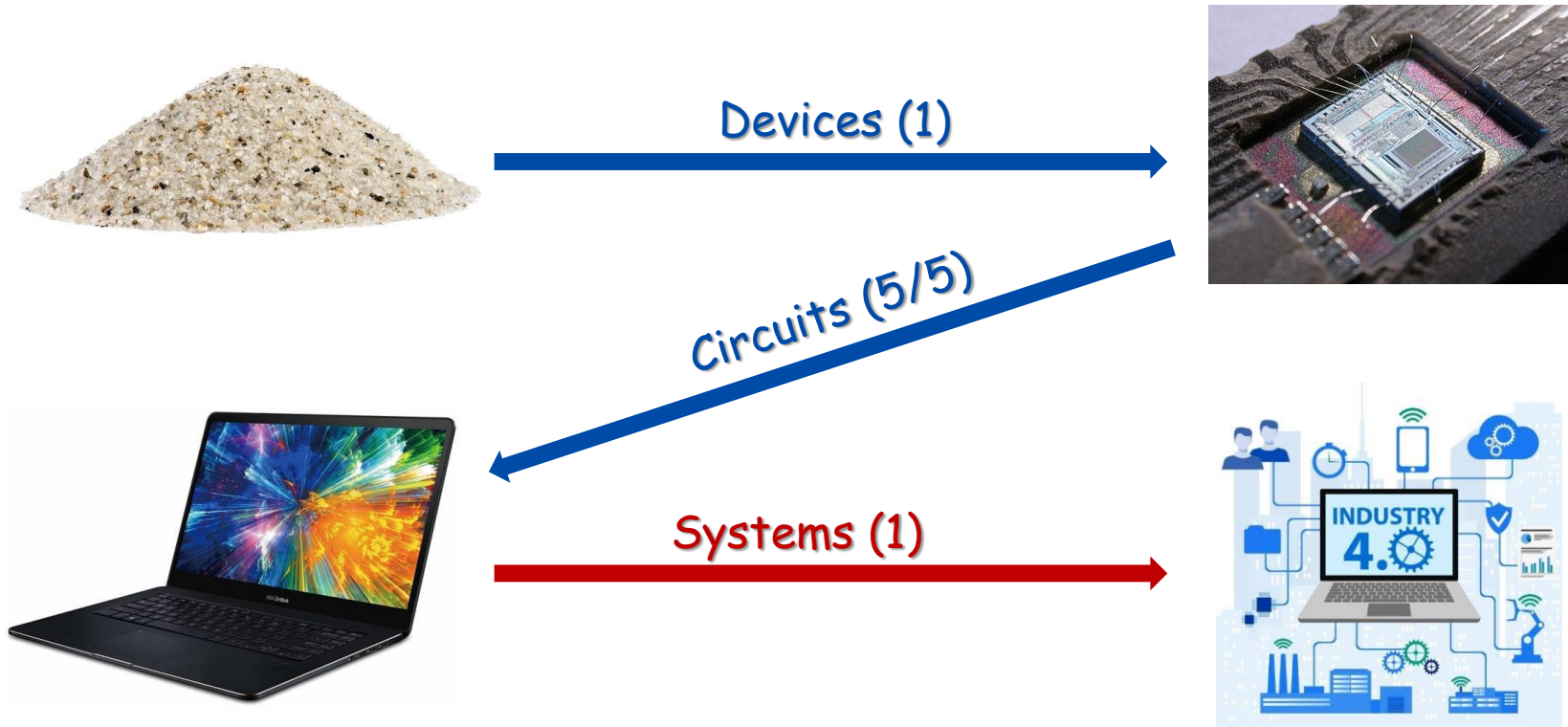
SI100B
**Introduction to Information
Science and Technology**
(Part 3: Electrical Engineering)

Lecture #8
Dynamic Systems and Control

Instructor: Haoyu Wang(王浩宇)

Apr 28th, 2023

The Theme Story



(Figures from Internet)

Study Purpose of Lecture #8

- 哲学三问
 - Who are you?
 - Where are you from?
 - Where are you going?

To answer those questions
throughout your life

你要到哪里去?
你从哪儿来?
你是谁?
哲学终极问题
门房大爷的问题



(Figures from Internet)

- In this lecture, we ask
 - What is **control** engineering?
 - What is **feedback** control system?
 - How does **PID** controller work?

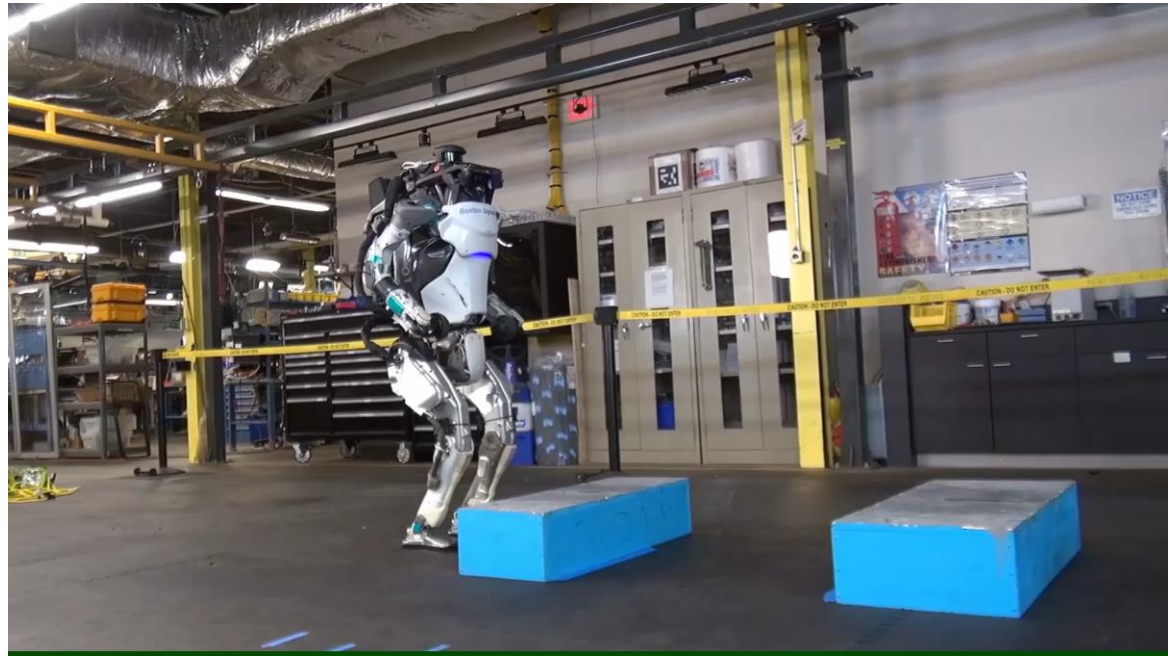


Lecture Outline

- **Control** and **connectivity** towards Industry 4.0
- Mathematical model of a dynamic system
- Feedback control system
 - Block diagram
 - Examples
- Controller design
 - **Proportional control**
 - **Integral control**
 - **Derivative control**

Application of Control Systems

- **Autonomous robots**
- Autonomous cars
- Quadcopters
- Self-balance robots
- Other more applications



(<https://www.youtube.com/watch?v=fRj34o4hN4I>)

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(<https://www.youtube.com/watch?v=t1Thdr3O5Qo>)

Application of Control Systems

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- **Quadcopters**
- Other more applications



(<https://www.youtube.com/watch?v=w2itwFJCgFQ>)

Definition of Control Systems

- Other more applications
 - Automatic assembly line
 - Space technology
 - Power systems
 - Smart transportation systems
 - Missile launching systems
 - ...
- **What is a control system?**



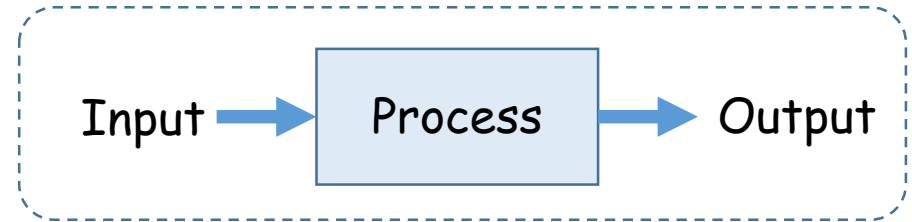
A control system is an interconnection of components forming a **system** configuration that will provide a desired system **response**.

—Richard C. Dorf & Robert H. Bishop, *Modern control systems*

Composition of Control Systems

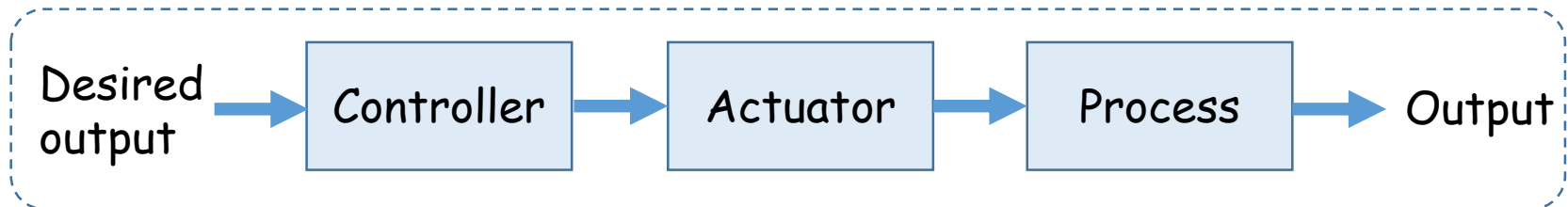
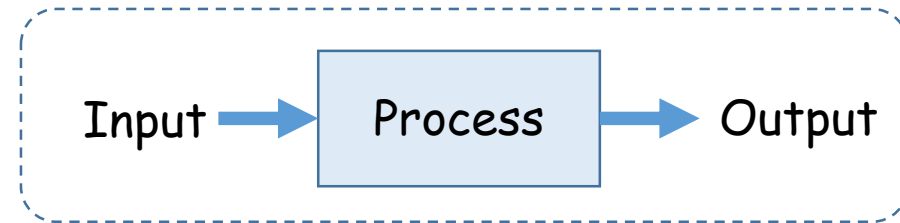
- **Linear system**

- Cause-effect relationship for the components
- Block diagram



Composition of Control Systems

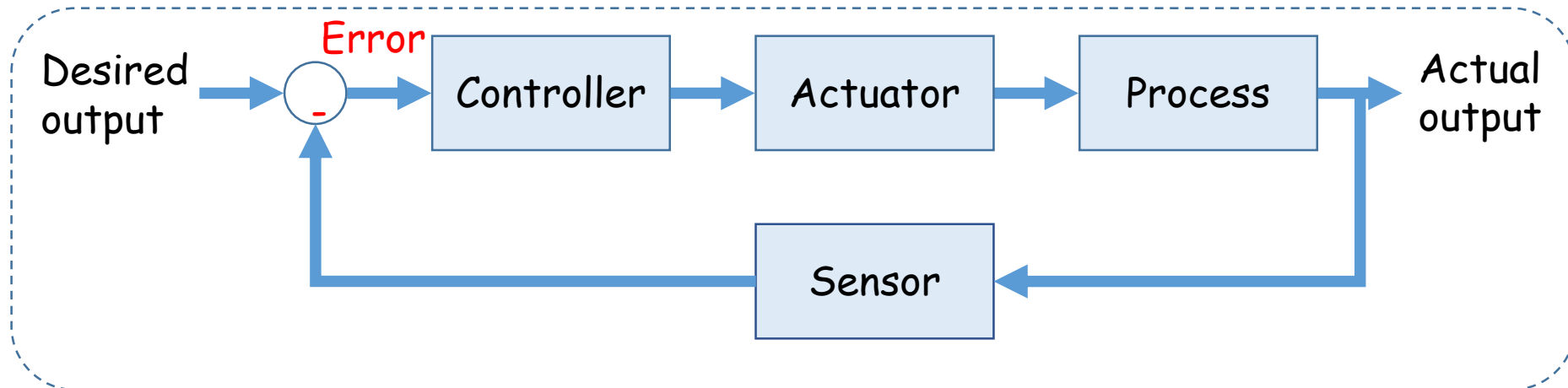
- Linear system
 - Cause-effect relationship for the components
 - Block diagram
- Open-loop control
 - Control the process **directly**



An open-loop control system uses a controller and an actuator to obtain the desired response, without using **feedback**.

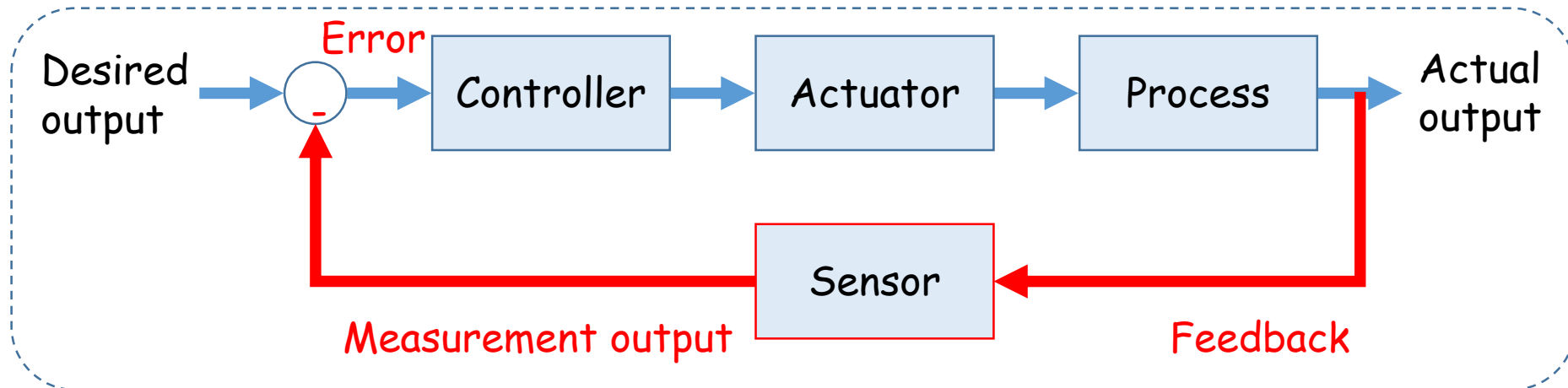
Composition of Control Systems

- **Closed-loop system**
 - Compare actual output with desire output



Composition of Control Systems

- **Closed-loop system**
 - Compare actual output with desire output

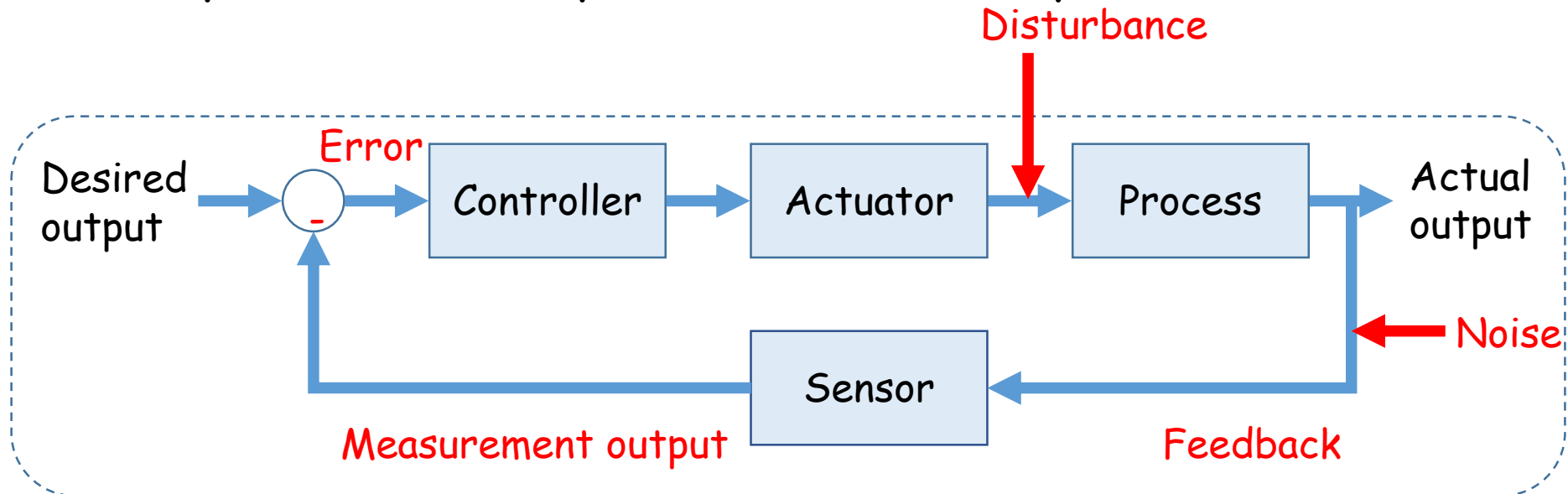


- Notice the difference: **error** based controller

Composition of Control Systems

- **Closed-loop system**

- Compare actual output with desire output



- An actual system also faced with disturbance and noise

Establishment of system model

- Start from a naive example
 - Consider a autonomous car start up and maintain a constant speed
 - Assuming:

Control variable

1° throttle angle cause a 10km/h change in speed

1° road grade cause a -5km/h change in speed

Disturbance



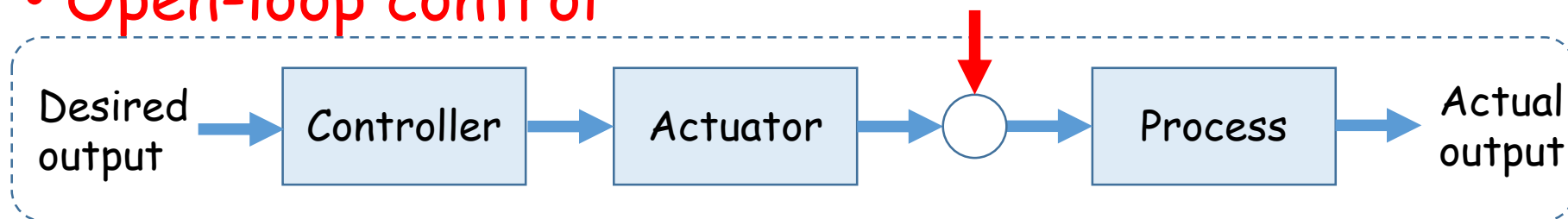
Establishment of system model

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• Open-loop control



Establishment of system model

- Start from a naive example
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 - Assuming:

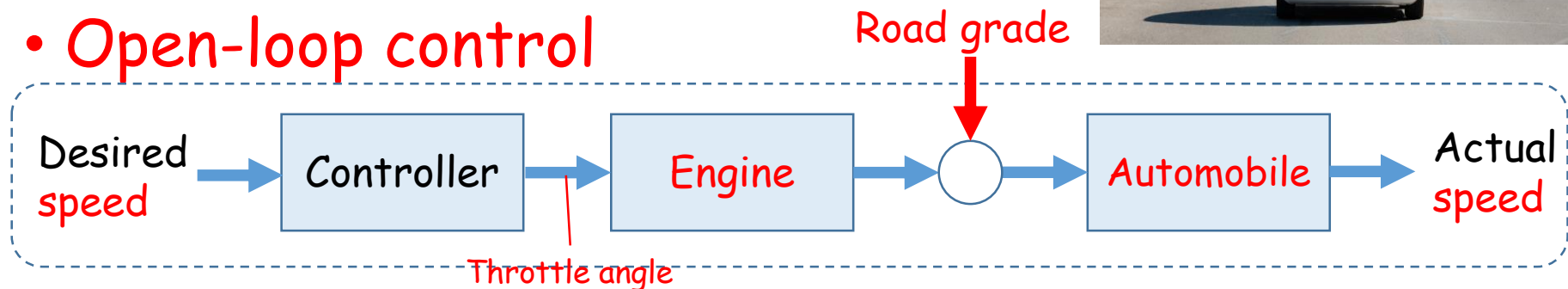
1° throttle angle cause a 10km/h change in speed
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Control variable

Disturbance



• Open-loop control



Establishment of system model

• Open-loop control

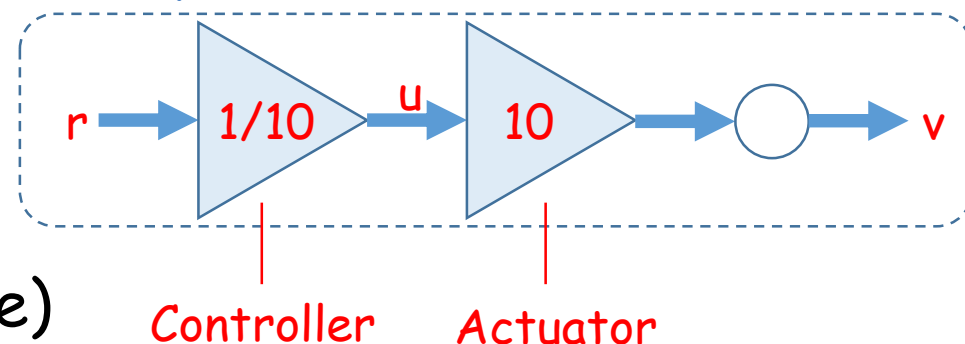
- Parameters definition

- r : desired speed (reference)

- u : throttle angle (control variable)

- w : road grade (disturbance)

- v : actual speed (output)



- If there is no external disturbance ($w=0$)

$$v = 10 * u, u = 1/10 * r \quad \longrightarrow \quad v = r$$

Assuming desired speed $r = 10$,

Actual speed $v = 10$



Establishment of system model

- Open-loop control

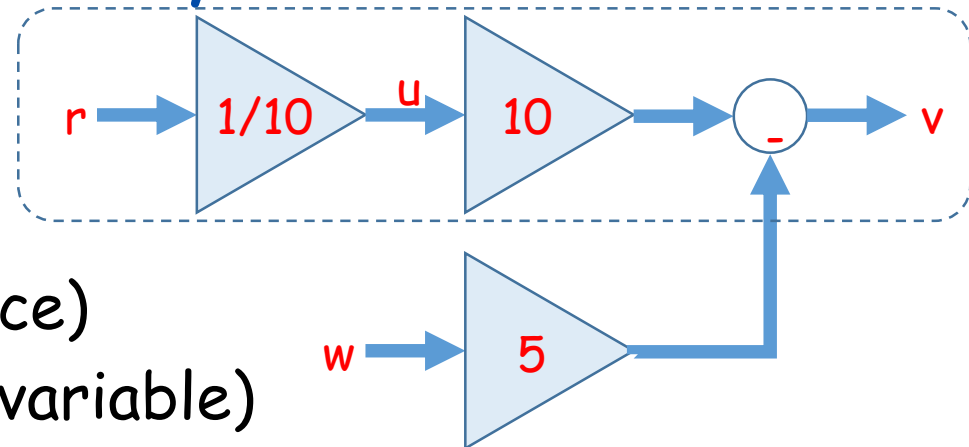
- Parameters definition

- r : desired speed (reference)

- u : throttle angle (control variable)

- w : road grade (disturbance)

- v : actual speed (output)



- If there exists external disturbance

$$v = 10 * u - 5 * w, \quad u = 1/10 * r \quad \longrightarrow \quad v = r - 5 * w$$

Assuming desired speed $r = 10$, and small disturbance $w = 1$

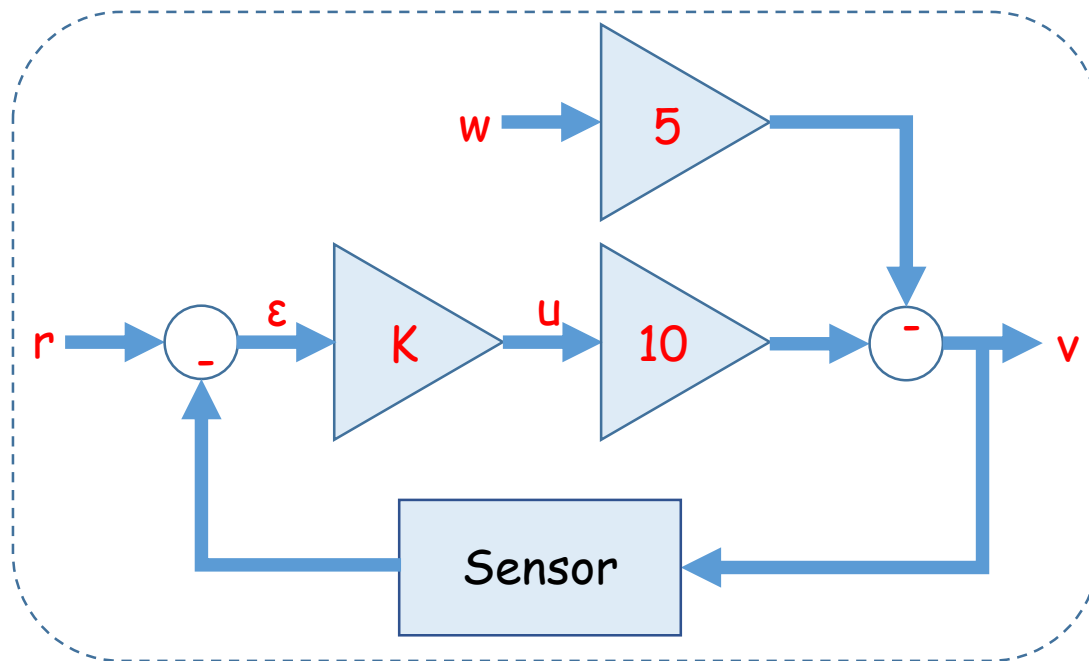
Actual speed $v = 5$



Establishment of system model

- **Closed-loop control**

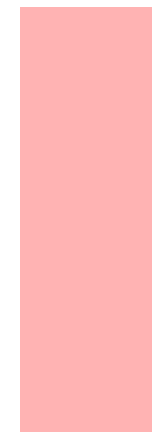
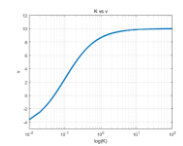
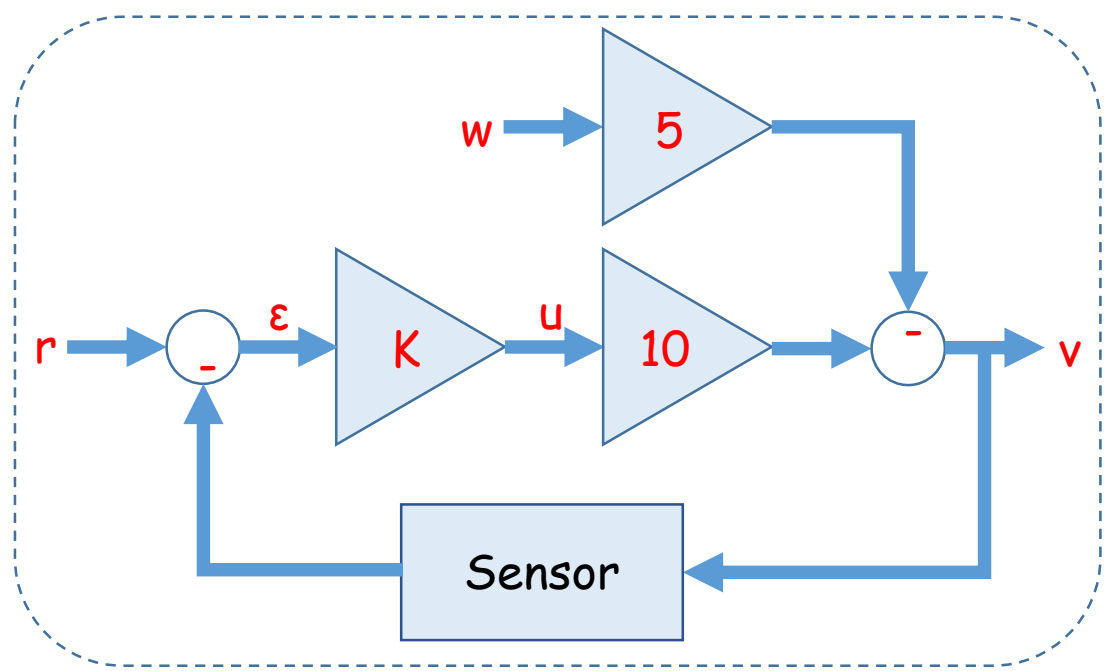
- ε : difference between actual speed and desired speed (error)
- K : coefficient (proportional coefficient)



Establishment of system model

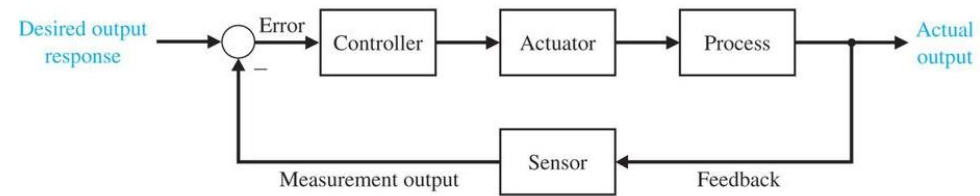
- **Closed-loop control**

- ϵ : difference between actual speed and desired speed (error)
- K : coefficient (proportional coefficient)

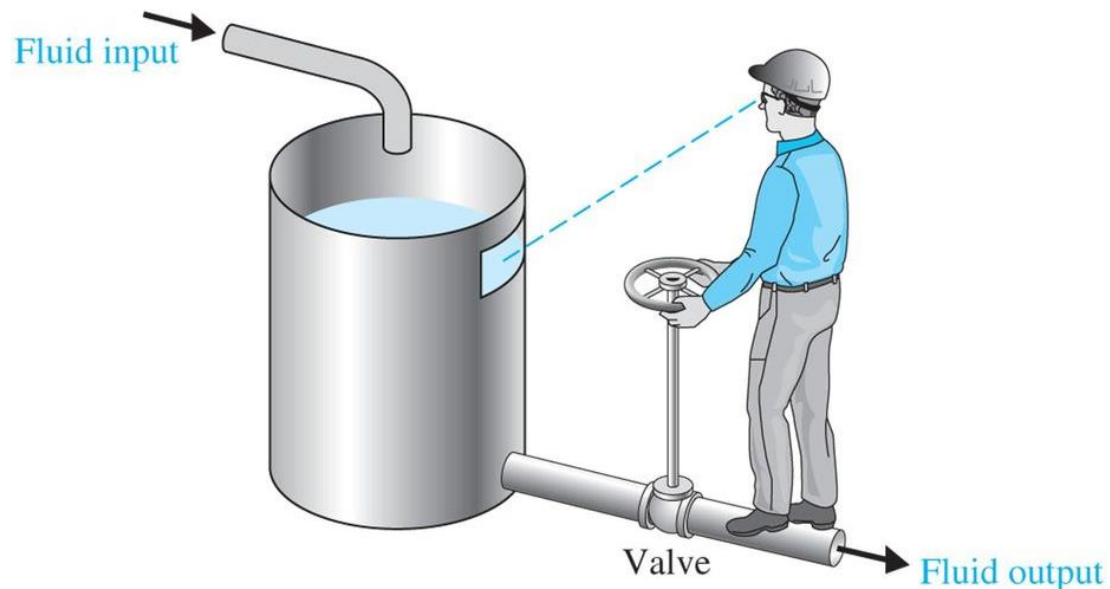


Example 1: manual control system

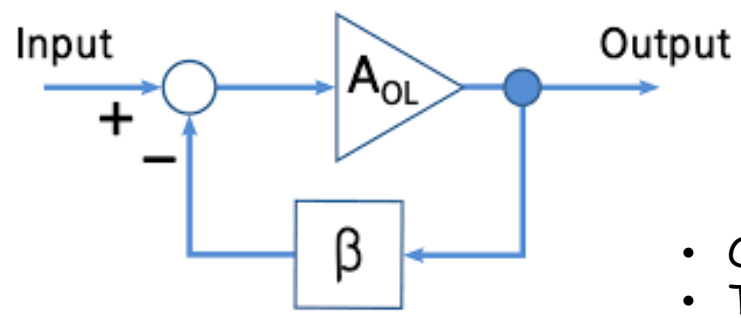
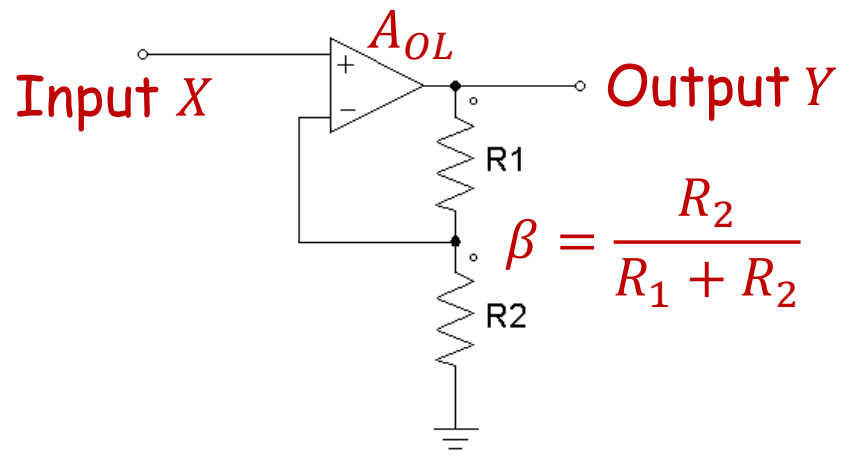
- In this manual control valve system, which one corresponds to the



- Process
- Actuator
- Sensor
- Controller
- Desire output
- Actual output
- Error

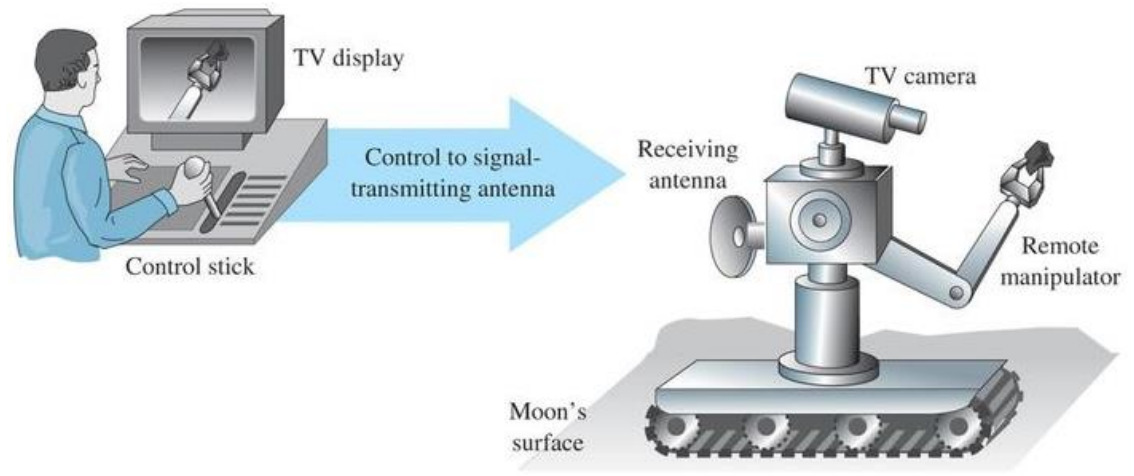


Example 2: Feedback amplifier



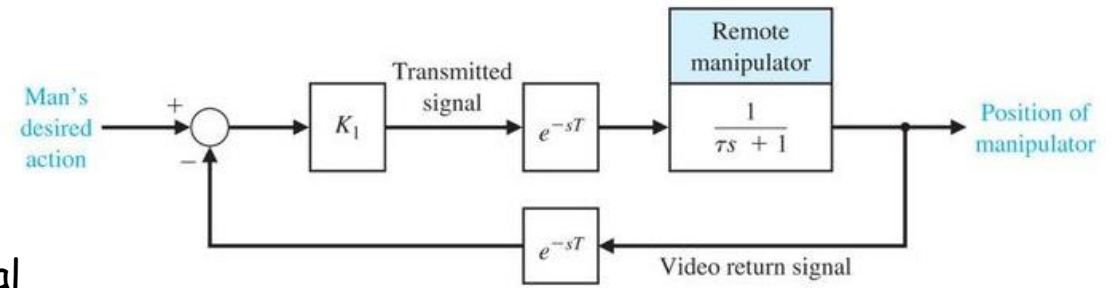
- Only considered the DC characteristics
- The AC characteristics are more complicated

Example 3: Moon robot



(a)

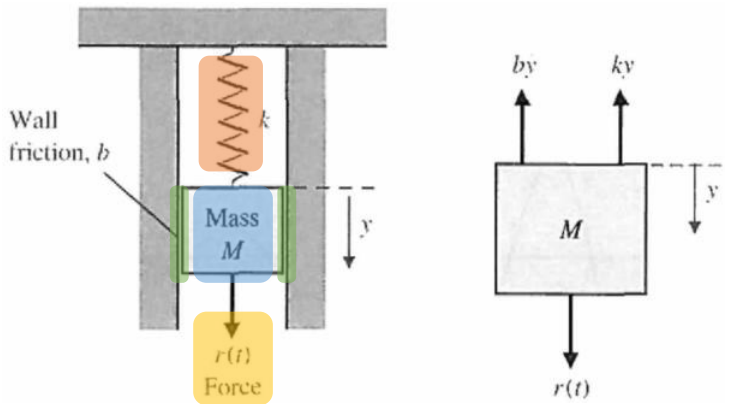
e^{-sT} models the time delay T in transmission of a communication signal



(b)

Differential equations for dynamic modeling

• Governing equation



Mass	Damping	Spring	Force
质量	阻尼	弹簧	力
$M \frac{d^2 y(t)}{dt^2}$	$+ b \frac{dy(t)}{dt}$	$+ ky(t)$	$= r(t)$

Table 2.2 Summary of Governing Differential Equations for Ideal Elements

Type of Element	Physical Element	Governing Equation	Energy E or Power Φ	Symbol
Inductive storage	Electrical inductance	$v_{21} = L \frac{di}{dt}$	$E = \frac{1}{2} Li^2$	
	Translational spring	$v_{21} = \frac{1}{k} \frac{dF}{dt}$	$E = \frac{1}{2} \frac{F^2}{k}$	
	Rotational spring	$\omega_{21} = \frac{1}{k} \frac{dT}{dt}$	$E = \frac{1}{2} \frac{T^2}{k}$	
	Fluid inertia	$P_{21} = I \frac{dQ}{dt}$	$E = \frac{1}{2} IQ^2$	
Capacitive storage	Electrical capacitance	$i = C \frac{dv_{21}}{dt}$	$E = \frac{1}{2} Cv_{21}^2$	
	Translational mass	$F = M \frac{dv_2}{dt}$	$E = \frac{1}{2} Mv_2^2$	
	Rotational mass	$T = J \frac{d\omega_2}{dt}$	$E = \frac{1}{2} J\omega_2^2$	
	Fluid capacitance	$Q = C_f \frac{dP_{21}}{dt}$	$E = \frac{1}{2} C_f P_{21}^2$	
Thermal capacitance	$q = C_t \frac{dT_2}{dt}$	$E = C_t T_2$		
Energy dissipators	Electrical resistance	$i = \frac{1}{R} v_{21}$	$\Phi = \frac{1}{R} v_{21}^2$	
	Translational damper	$F = bv_{21}$	$\Phi = bv_{21}^2$	
	Rotational damper	$T = b\omega_{21}$	$\Phi = b\omega_{21}^2$	
	Fluid resistance	$Q = \frac{1}{R_f} P_{21}$	$\Phi = \frac{1}{R_f} P_{21}^2$	
	Thermal resistance	$q = \frac{1}{R_t} T_{21}$	$\Phi = \frac{1}{R_t} T_{21}^2$	

Frequency-domain expressions

$$M \frac{d^2 y(t)}{dt^2} + b \frac{dy(t)}{dt} + ky(t) = r(t)$$

- Transfer function
 - Describing the dynamic relationship of the system in the **frequency domain**

Laplace
transform

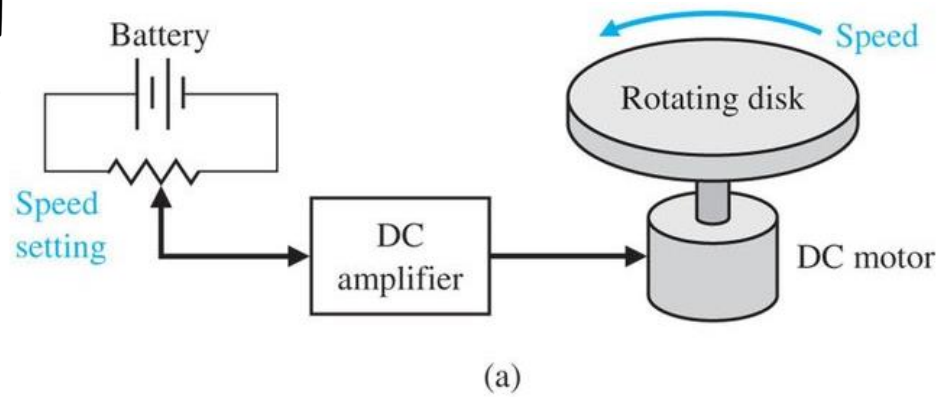
$$Ms^2 Y(s) + bsY(s) + kY(s) = R(s)$$

Input/output
relation

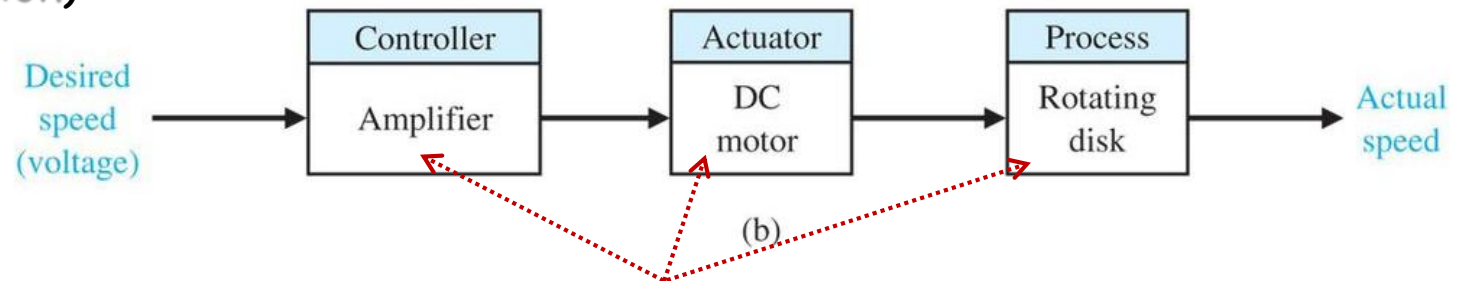
$$\frac{\text{Output}}{\text{Input}} = G(s) = \frac{Y(s)}{R(s)} = \frac{1}{Ms^2 + bs + k}$$

Block diagram

A practical rotational speed control system

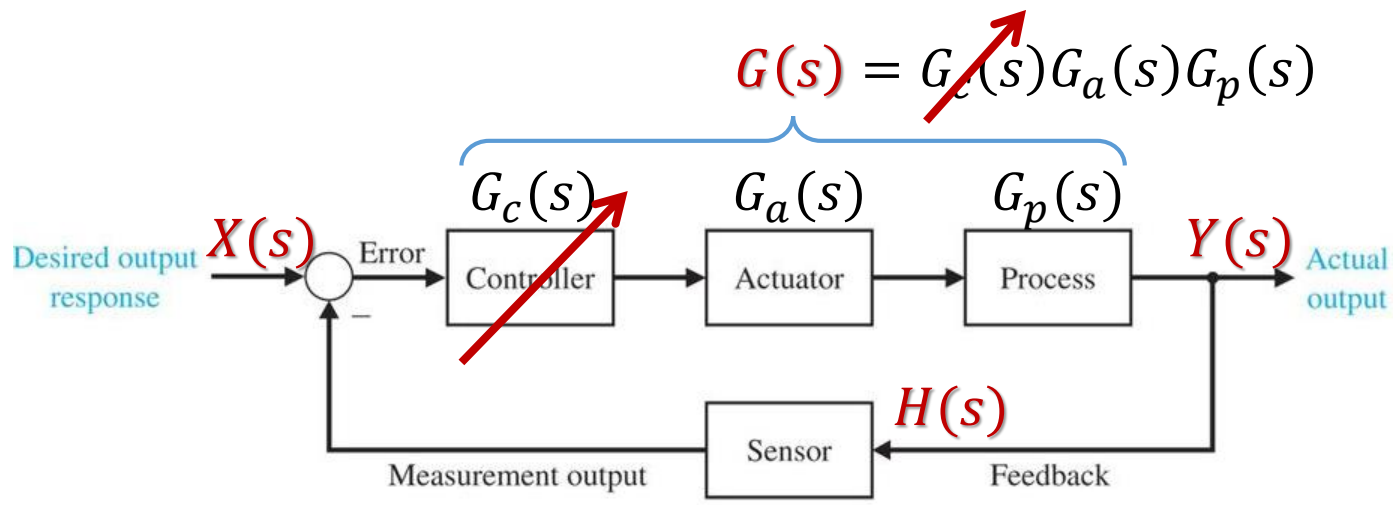


The corresponding block diagram (abstraction)



Representing a time-domain or frequency-domain (mathematical) model

Mathematical model of feedback control system



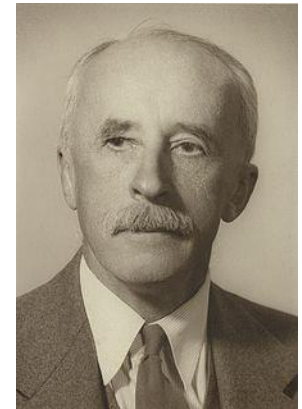
Tuning the close-loop system characteristics by changing the controller characteristics

Open-loop gain

Close-loop gain

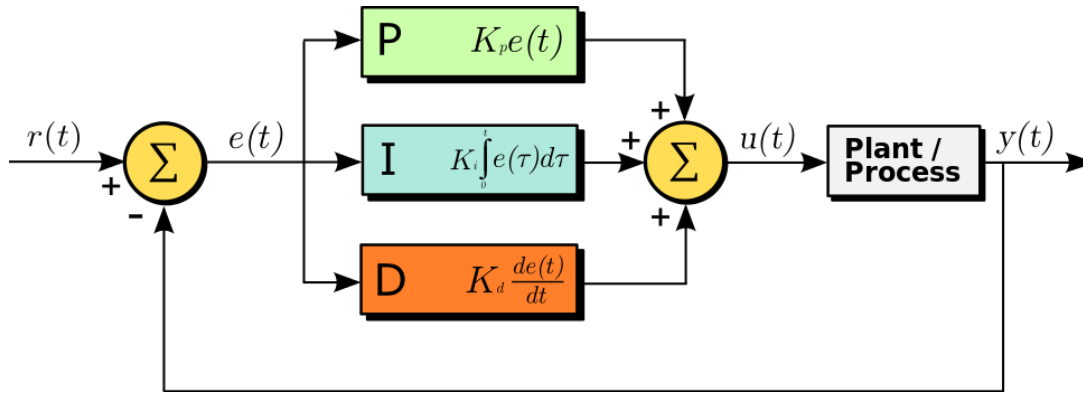
PID controller

- A Brief History of PID Control
- 1890's, PID (Proportional - Integral - Derivative) Control, originally developed in the form of motor governors, which were manually adjusted
- 1922, the first theory of PID Control was published by Nicolas Minorsky, who was working for the US Navy
- 1940's, the first papers regarding PID tuning appeared
 - there are several hundred different rules for tuning PID controllers (See Dwyer, 2009)
- Nowadays, **97%** of regulatory controllers utilize PID feedback
 - based on a survey of over eleven thousand controllers in the refining, chemicals and pulp and paper industries (see Desborough and Miller, 2002).

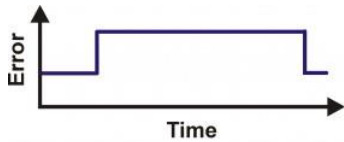


Nicolas Minorsky
(1885- 1970)
a Russian American
control theory
mathematician,
engineer and applied
scientist

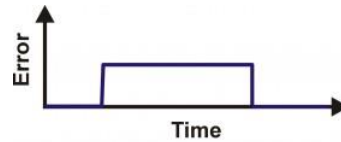
PID controller



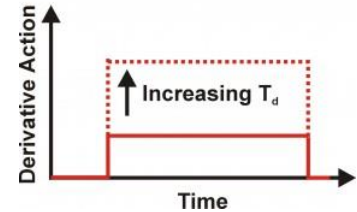
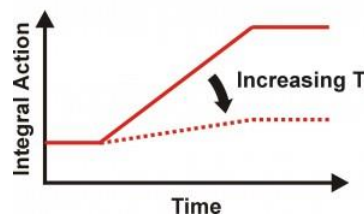
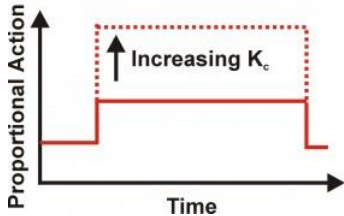
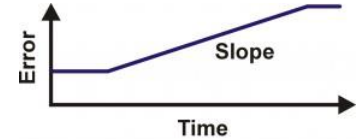
Current error



Past error



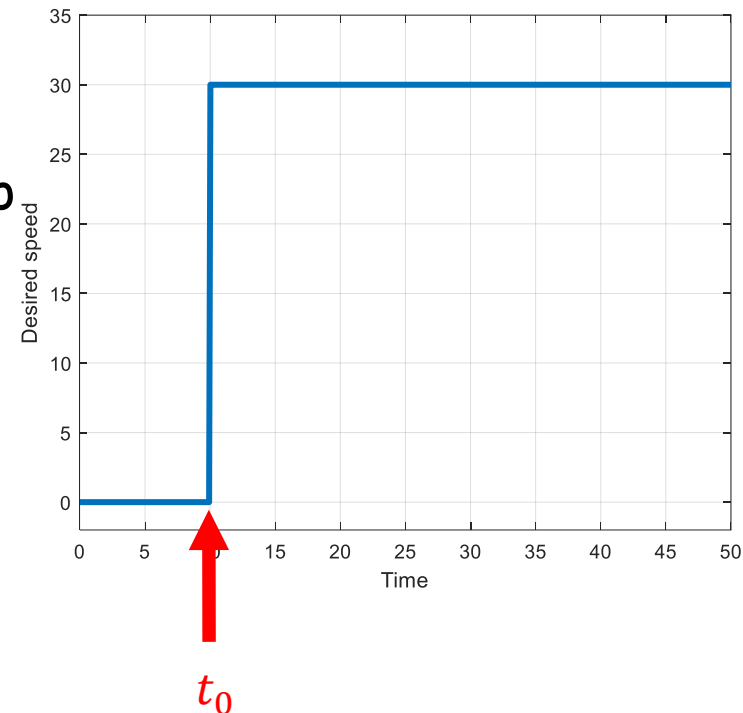
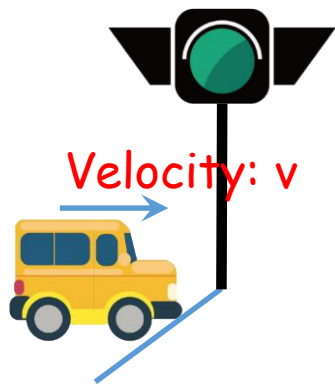
Future error



Composition of PID controller

• Case 1

- Autonomous car stops at a red light
- At t_0 , light turns green and car starts up
- And finally reaches desired speed
- Desired speed is a **step function** at t_0

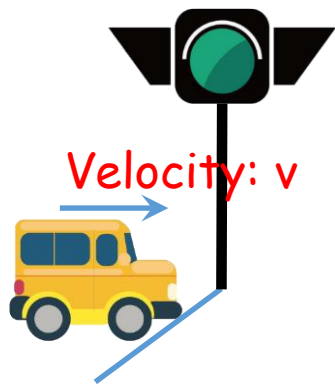
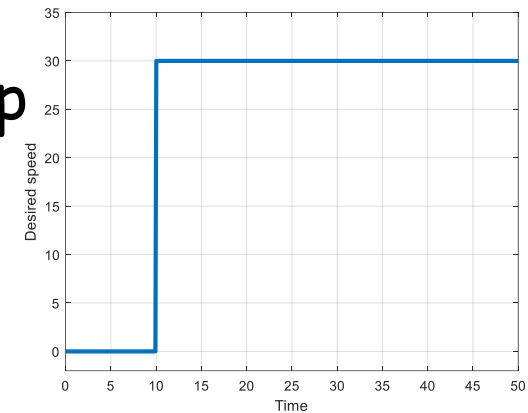


Composition of PID controller

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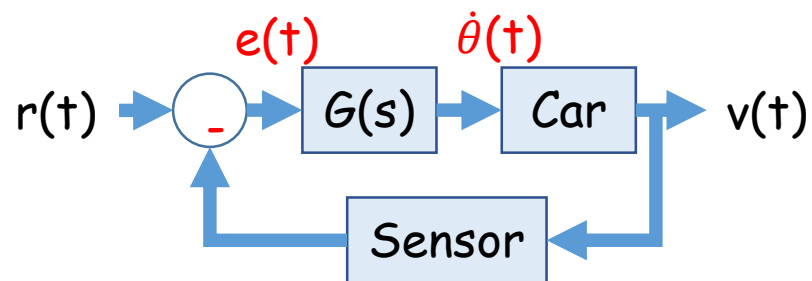
- Consider a proportional control only



$$G(s) = K_p, K_p > 0$$

$$\dot{\theta}(t) = K_p * e(t)$$

θ represents the throttle angle
and $\dot{\theta}$ is the derivative, which represents the **change** in speed



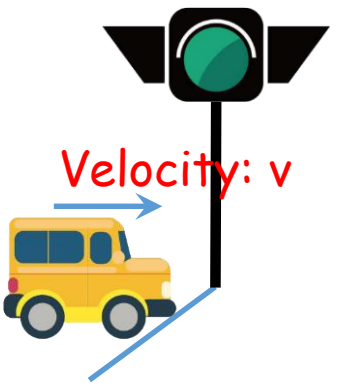
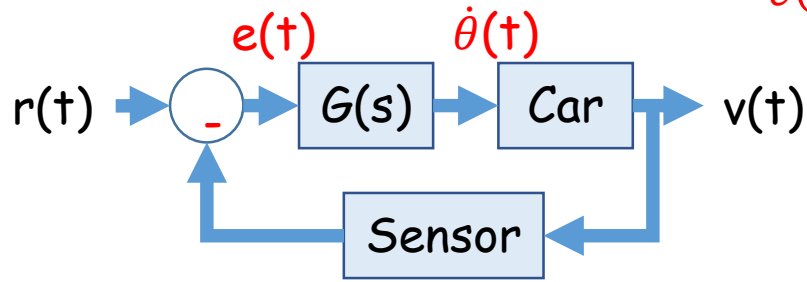
Composition of PID controller

- Case 1

- Consider a proportional control only

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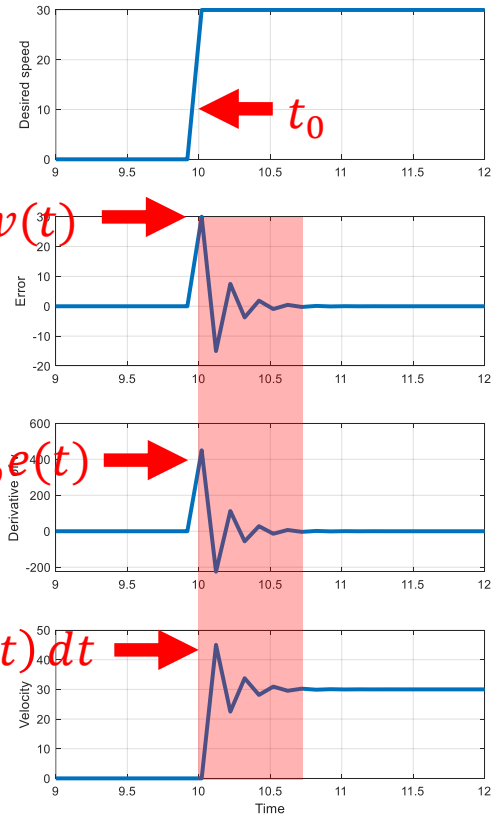
$$\dot{\theta}(t) = K_p * e(t)$$



$$e(t) = r(t) - v(t)$$

$$\dot{\theta}(t) = K_p e(t)$$

$$v(t) = \int \dot{\theta}(t) dt$$



Notice the oscillation in velocity, due to an aggressive K_p

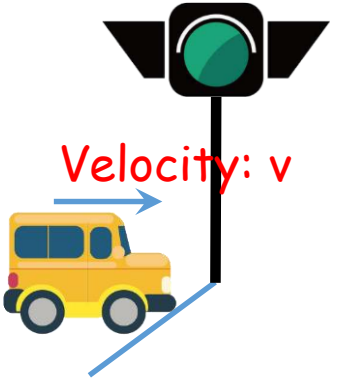
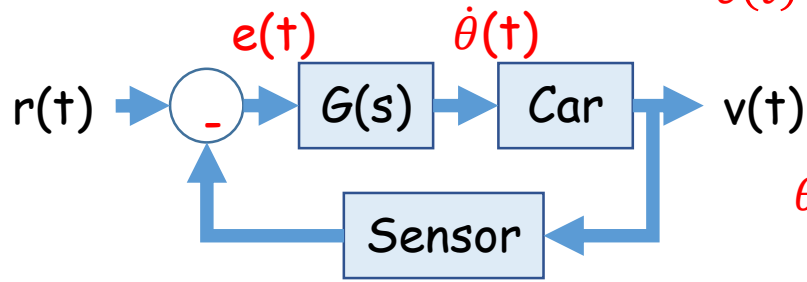
Composition of PID controller

- Case 1

- Consider a proportional control only

$$G(s) = K_p, K_p > 0$$

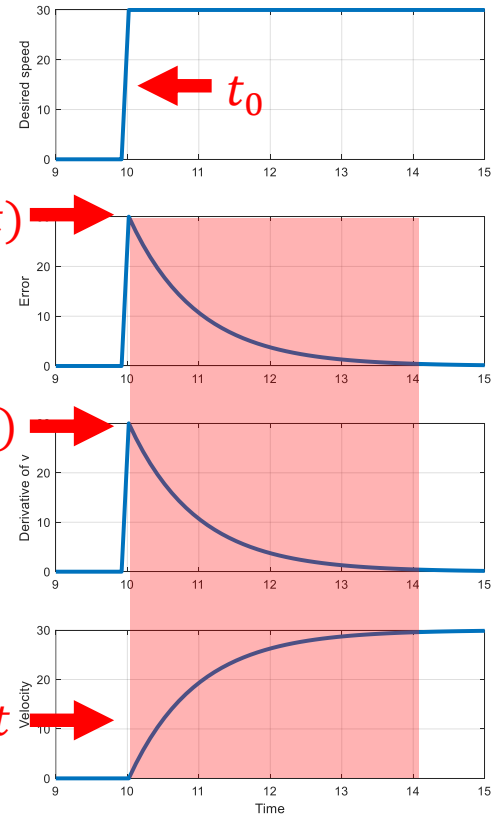
$$\dot{\theta}(t) = K_p * e(t)$$



$$e(t) = r(t) - v(t)$$

$$\dot{\theta}(t) = K_p e(t)$$

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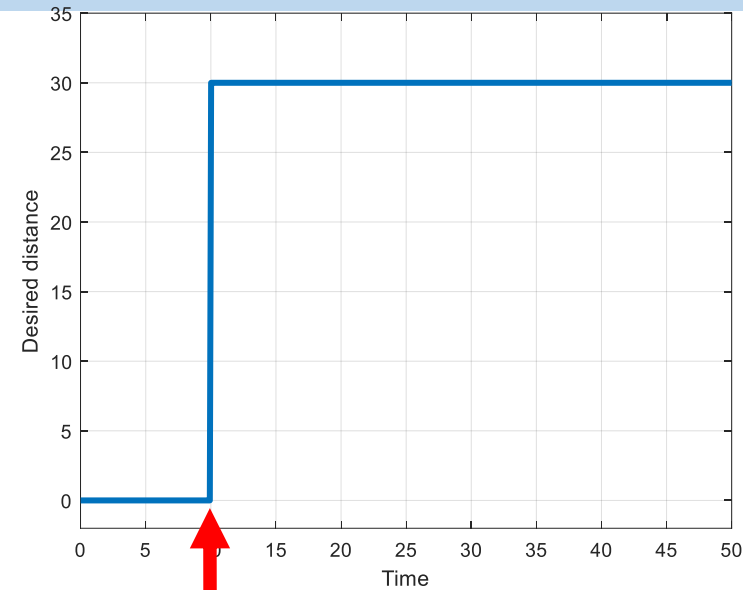


Smaller K_p reduces oscillation, but is more time-consuming

Composition of PID controller

• Case 2

- Autonomous car stops at a red light
- Another red light some distance away
- At t_0 , light turns green and car starts up
- And finally stops at the second light



- **Desired distance** is a step function at t_0



Composition of PID controller

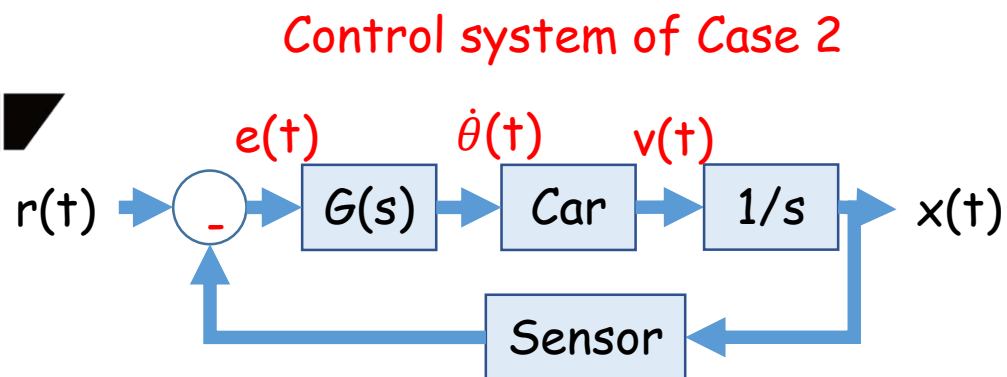
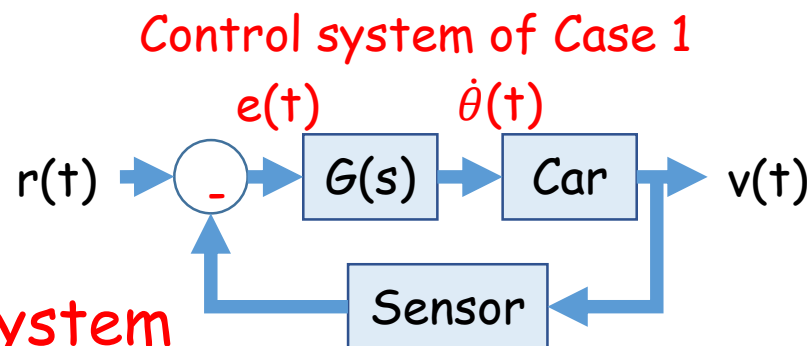
• Case 2

- If proportional control only

$$G(s) = K_p, K_p > 0$$

$$\dot{\theta}(t) = K_p * e(t)$$

- Notice the change in **control system**



Composition of PID controller

- Case 2

- If proportional control only

$$G(s) = K_p, K_p > 0$$

$$\dot{\theta}(t) = K_p * e(t)$$

- On previous experience, choose small K_p

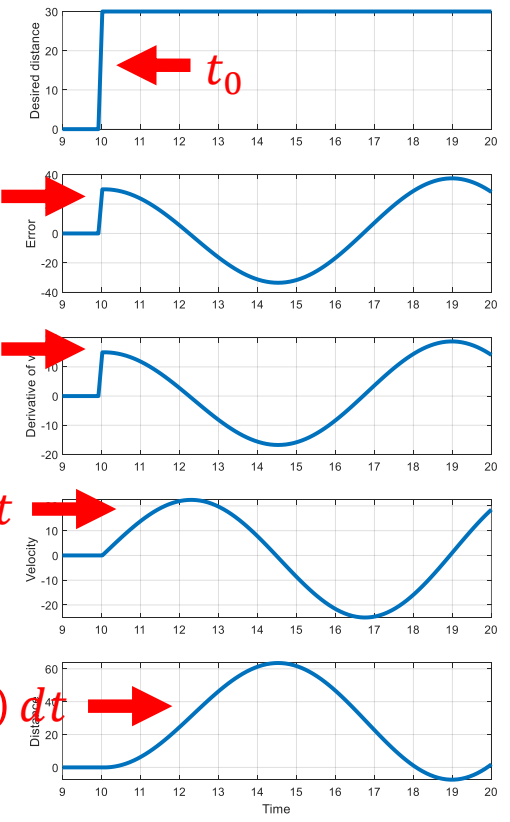


$$e(t) = r(t) - x(t)$$

$$\dot{\theta}(t) = K_p e(t)$$

$$v(t) = \int \dot{\theta}(t) dt$$

$$x(t) = \int v(t) dt$$



Why is this happening?

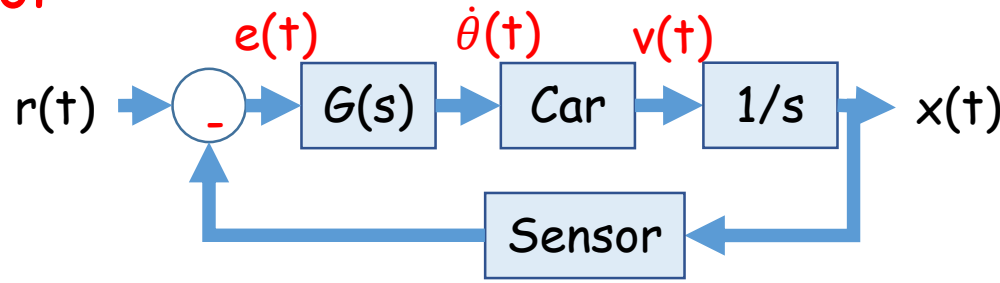
Composition of PID controller

- Case 2

- Introduce derivative control

$$G(s) = K_p + K_d \cdot s, \quad K_p, K_d > 0$$

$$\dot{\theta}(t) = K_p \cdot e(t) + K_d \cdot \dot{e}(t)$$



- Therefore, proportional-derivative (PD) control



Composition of PID controller

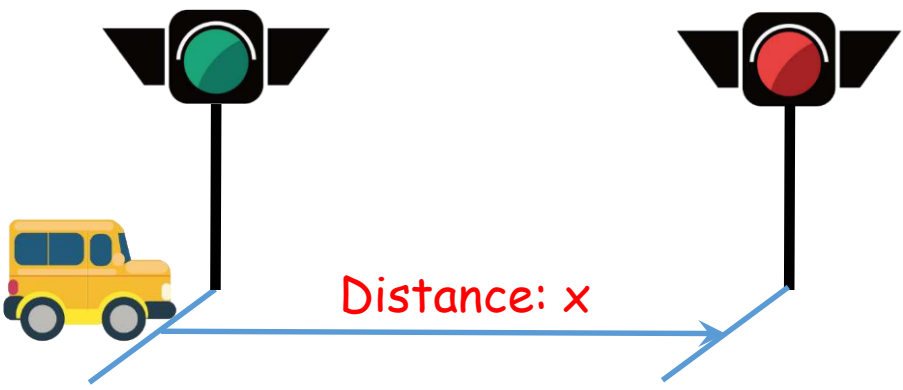
- Case 2

- Introduce derivative control

$$G(s) = K_p + K_d \cdot s, \quad K_p, K_d > 0$$

$$\dot{\theta}(t) = K_p \cdot e(t) + K_d \cdot \dot{e}(t)$$

- Therefore, proportional-derivative (PD) control

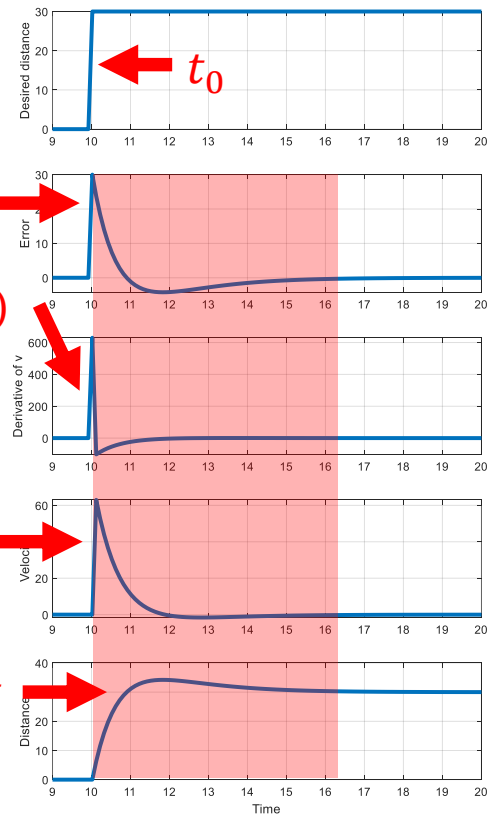


$$e(t) = r(t) - x(t)$$

$$\dot{\theta}(t) = K_p e(t) + K_d \dot{e}(t)$$

$$v(t) = \int \dot{\theta}(t) dt$$

$$x(t) = \int v(t) dt$$

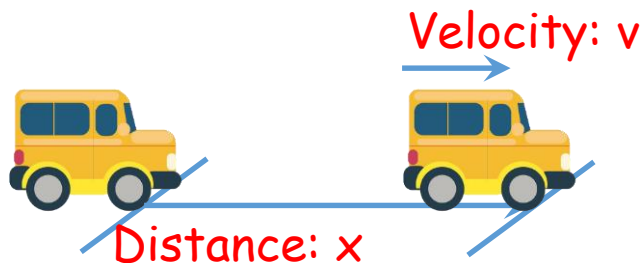
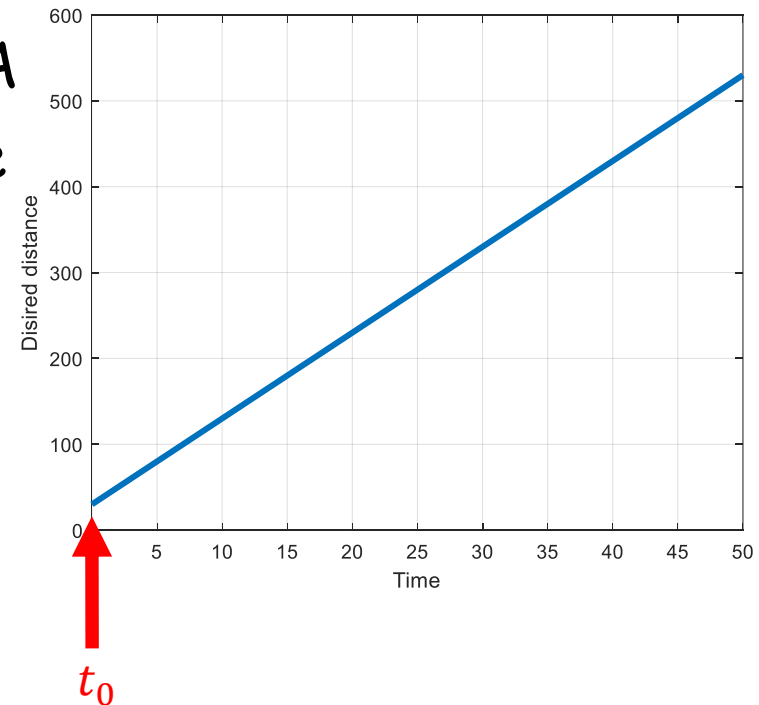


Similarly, oscillation exist (inevitable), but much smaller

Composition of PID controller

• Case 3

- Car A runs at a constant speed
- Car B starts up to catch up with A
- Finally two cars drive side by side
- **Desired distance** is a linear function
- And what is the **control variable** this time?



Composition of PID controller

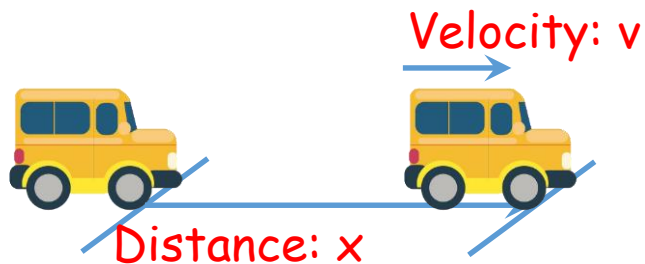
- Case 3

- If still only consider proportional control

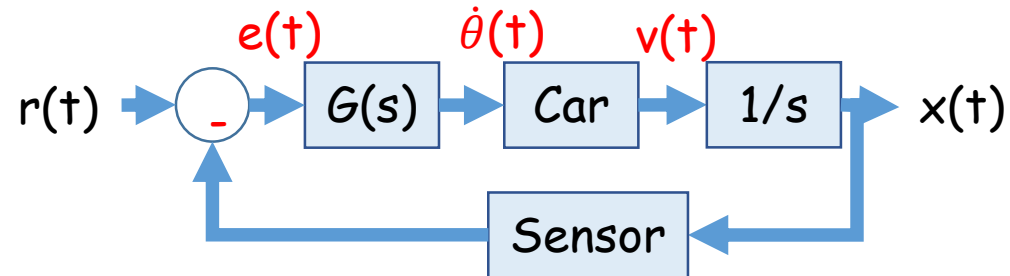
$$G(s) = K_p, K_p > 0$$

$$\theta(t) = K_p * e(t)$$

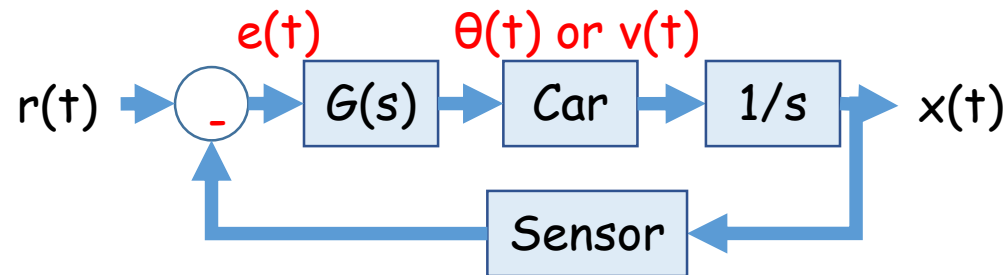
- Notice this time the control variable is **velocity (or throttle angle θ)**



Control system of Case 2



Control system of Case 3



Composition of PID controller

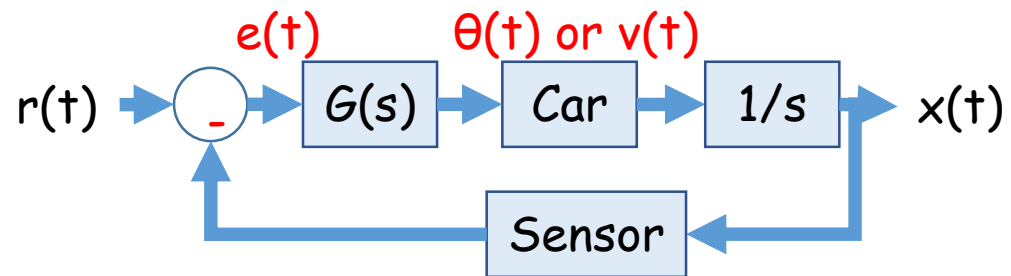
• Case 3

- If still only consider proportional control

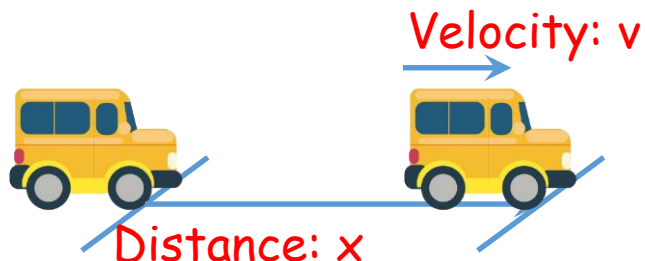
$$G(s) = K_p, K_p > 0$$

$$v(t) = K_p * e(t)$$

Control system of Case 3



- On previous experience, choose small K_p



Composition of PID controller

• Case 3

- If still only consider proportional control

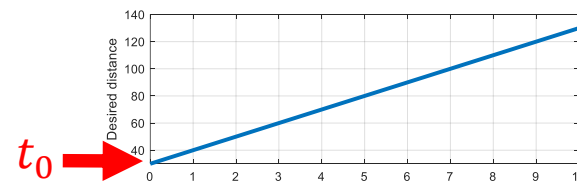
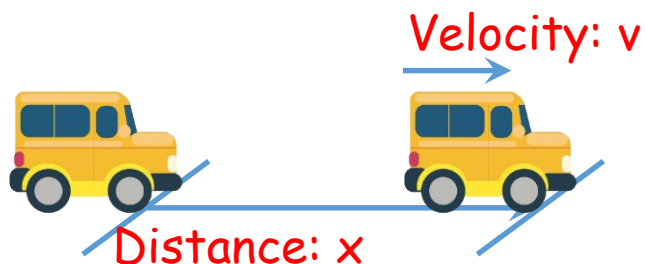
$$G(s) = K_p, K_p > 0$$

$$v(t) = K_p * e(t)$$

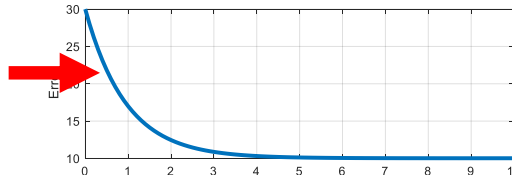
- On previous experience, choose small K_p

- Cannot catch up

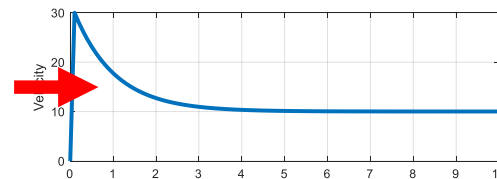
- Final $v = K_p * e(t)$ and $e(t)$ maintains



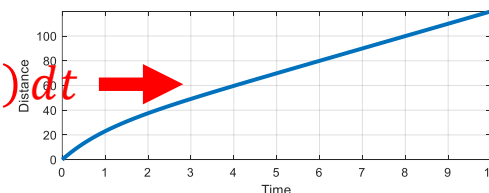
$$e(t) = r(t) - x(t)$$



$$v(t) = K_p e(t)$$



$$x(t) = \int v(t) dt$$



Composition of PID controller

- Case 3

- Introduce integral control

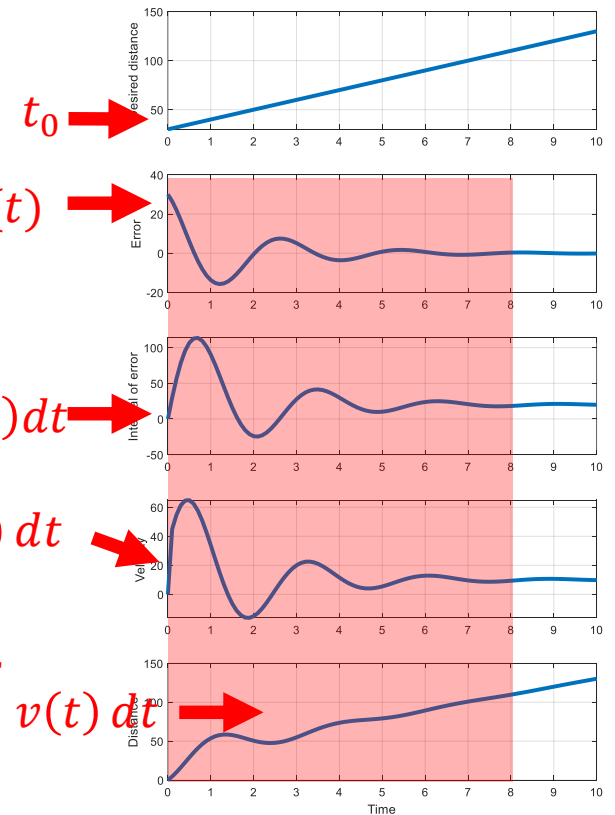
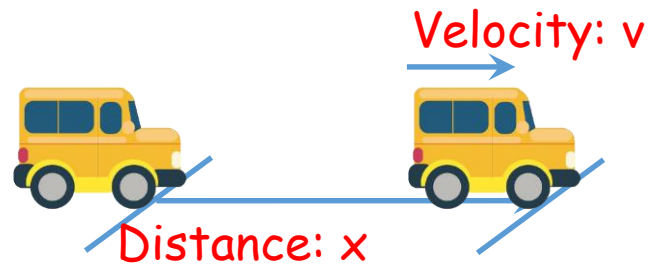
$$G(s) = K_p + K_i \cdot (1/s), \quad K_p, K_i > 0$$

$$v(t) = K_p \cdot e(t) + K_i \int e(t) dt$$

- Therefore, proportional-integral (PI) control

$$v(t) = K_p e(t) + K_i \int e(t) dt$$

$$x(t) = \int v(t) dt$$



$$e(t) = r(t) - x(t)$$

Oscillation inevitable, and integral part increases overshoot

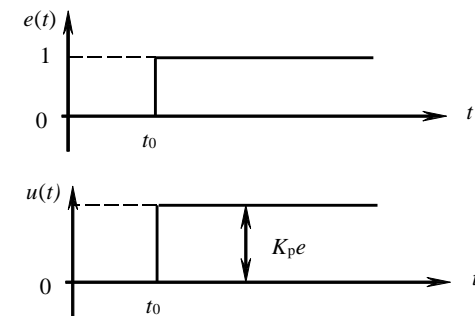
Mathematical analysis of PID controller

• P Control

- Proportional control (P): accounts for present values of the error

- U — control signal
- K_p — proportional gain
- e — error signal

- In the Laplace domain



Step response for P control

• Pros&Cons

- Rapid response to track the error signal
- Steady-state error
- Prone to be unstable for large K_p

- Proportional control is always present, either by itself, or allied with derivative and/or integral control

Mathematical analysis of PID controller

• I Control

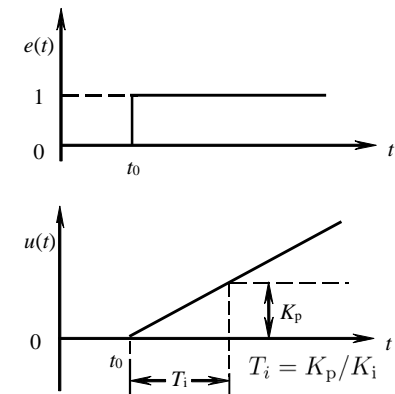
- Integral control (I): accounts for past values of the error

- U — control signal
- K_i — integral gain
- e — error signal

- In the Laplace domain

• Pros&Cons

- Eliminates the steady-state error that occurs with pure P control
- Prone to cause the present value to overshoot the setpoint (responds to accumulated errors from the past)



Step response for I control

Mathematical analysis of PID controller

• D Control

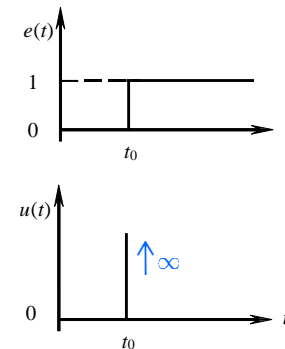
- Derivative control (D): accounts for possible future trends of the error

- U — control signal
- K_d — derivative gain
- e — error signal

- In the Laplace domain

• Pros&Cons

- Predicts system behavior and thus improves settling time/transient response and stability of the system
- Helps reduce overshoot, but amplifies noise (derivative kick)
- Seldom used in practice, 80% of the employed PID controllers have the D part switched-off (see Ang et al., 2005)

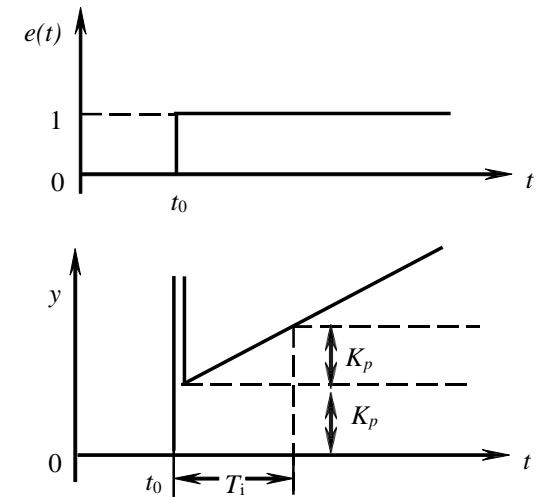


Step response for D control

Mathematical analysis of PID controller

- PID Control
- Proportional integral derivative control (PID): a combination of P, I and D control

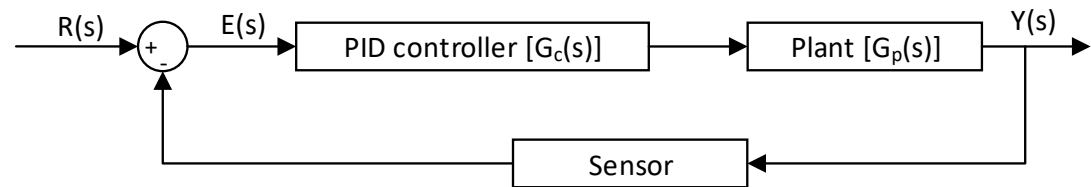
- In the Laplace domain



Step response for PID control

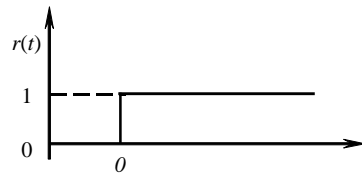
Mathematical analysis of PID controller

• Steady-state error



Input signal: unit step signal

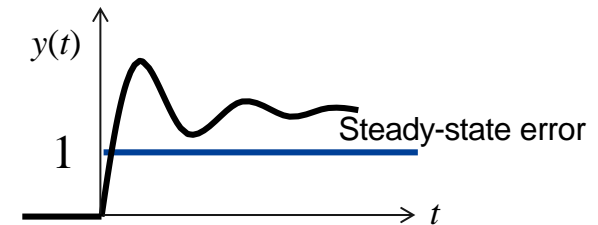
Close-loop gain for PID



Plant: 2nd order system

Mathematical analysis of PID controller

- Steady-state error
- P control
- Final-value theorem



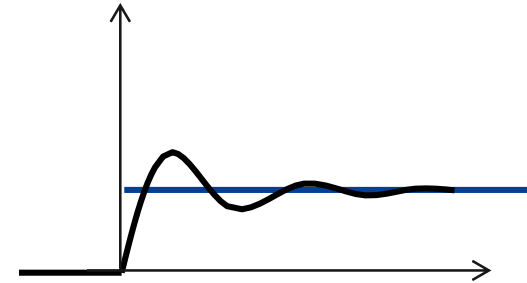
- Steady-state error always occurs;
- Larger K_p makes steady state error goes to zero

Mathematical analysis of PID controller

- Steady-state error
- PD control
- Final-value theorem
 - Steady-state error remains
 - D control does not track error, only affect the rate of change

Mathematical analysis of PID controller

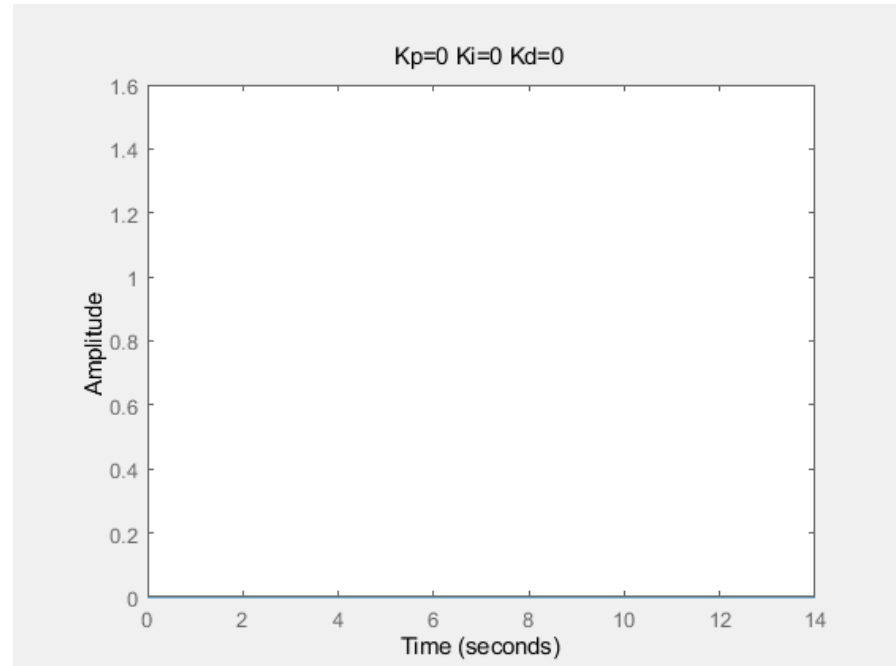
- Steady-state error
- PI control
- Final-value theorem



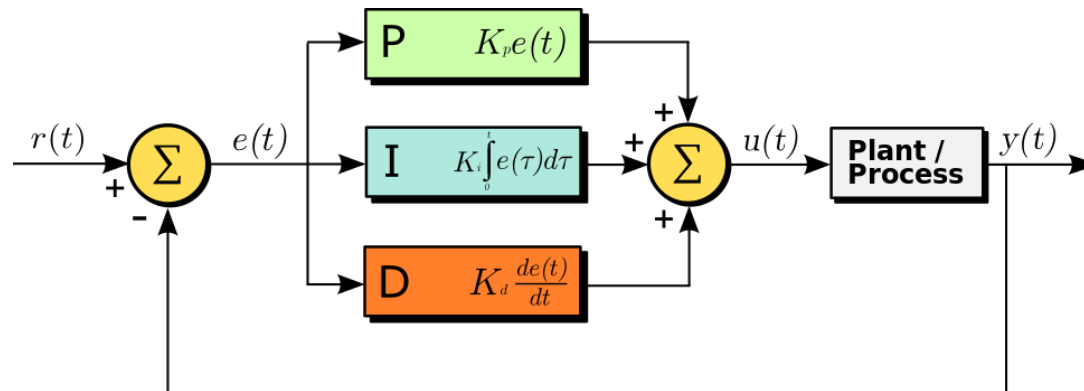
- Steady-state error is zero for a step reference, even for small K_i (just takes longer to reach steady state).

PID controller

- Steady-state error
- PID control
- Final-value theorem

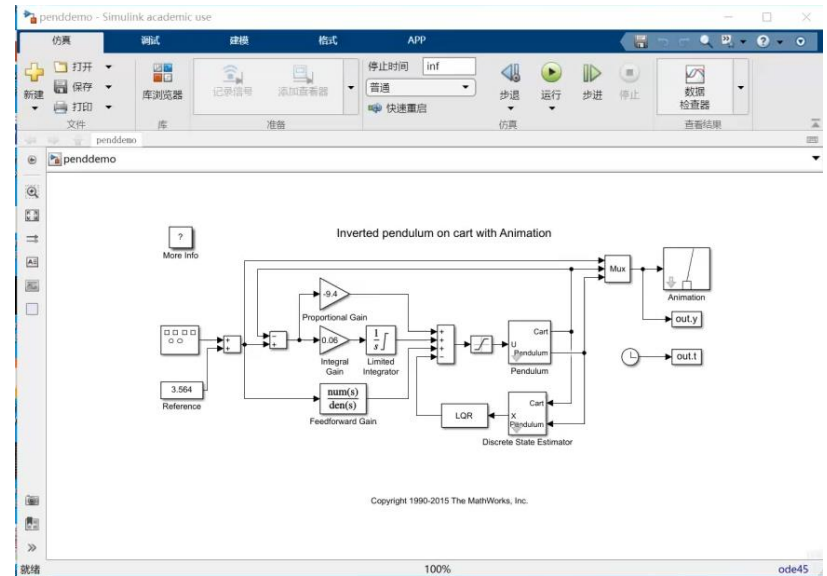
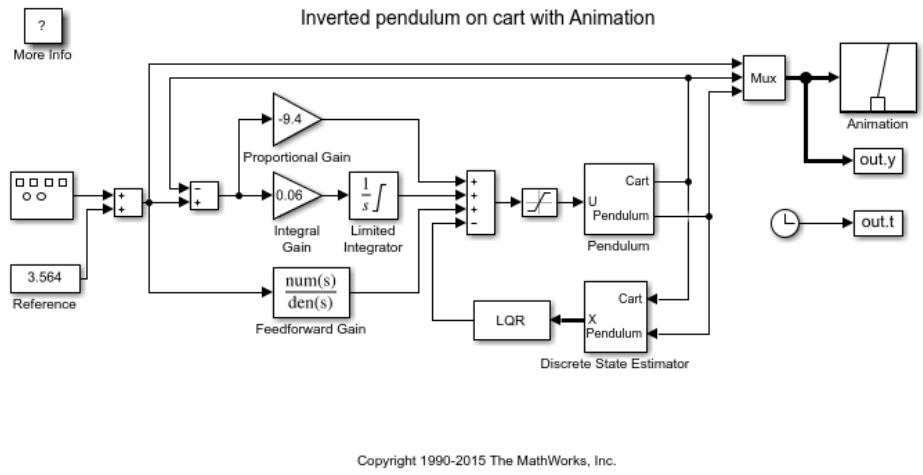


Summary of PID controller



PID gain	Overshoot	Settling-time	Steady-state error
Increasing K_p	Increases	Minimal impact	Decreases
Increasing K_i	Increases	Increases	Zero error
Increasing K_d	Decreases	Decreases	No impact

Inverted pendulum example in Matlab



Key in the command:

```
>> openExample('simulink_general/penddemoExample')
```